

## A note on a necessary condition for optimality

DAVID DI RUSCIO†

*Keywords:* Linear optimal control, multivariable systems, pole placements, eigenvalues, control theory.

A necessary condition is derived for the optimality of a linear multivariable feedback control system with respect to a quadratic performance index of infinite settling time.

### 1. Introduction

In linear quadratic system design the relation between the quadratic weights and the dynamic characteristics of the closed-loop system is of interest. This problem has been solved for a second order system (Di Ruscio and Balchen, 1990). In the general case, very little is known about these relations.

Let  $\lambda_i, i = 1, \dots, n$  be the open-loop poles and  $s_i, i = 1, \dots, n$  be the closed-loop poles. MacFarlane (1970) presented an inequality between the product of the open-loop poles and the product of the closed-loop poles,

$$\prod_{i=1}^n |s_i| \geq \prod_{i=1}^n |\lambda_i|$$

Koussiouris (1982) (later corrected by Amin, 1984) presented an inequality between the sum of squares of the open-loop poles and closed-loop system poles,

$$\sum_{i=1}^n s_i^2 \geq \sum_{i=1}^n \lambda_i^2$$

These relations are, as we can see, conservative because the quadratic weights do not appear in the relations. In this paper an exact relation between the open-loop and closed-loop system poles is presented. We will show that the relation by Amin and Koussiouris is a special case of our relation.

### 2. Theory

Let  $A$  be the  $n \times n$  real state system matrix and  $B$  the  $n \times r$  real control input matrix. Let  $Q$  be the  $n \times n$  real symmetric state weight matrix and  $P$  the  $r \times r$  real symmetric positive definite control input weight matrix. Then we have the following theorem.

#### *Theorem*

If  $s_i, i = 1, \dots, n$  are the closed-loop system poles and  $\lambda_i, i = 1, \dots, n$  are the open-loop system poles, then  $s_i, i = 1, \dots, n$  are related to  $A$  or  $\lambda_i, Q$  and the positive semidefinite matrix  $H = BP^{-1}B^T$  by the following equality,

$$\sum_{i=1}^n s_i^2 = \text{tr}(A^2) + \text{tr}(HQ) \quad (1)$$

---

Received 1 August, 1990.

† Division of Engineering Cybernetics, Norwegian Institute of Technology, N-7034 Trondheim, Norway.

or equivalently

$$\sum_{i=1}^n \{(\operatorname{Re} s_i)^2 - (\operatorname{Im} s_i)^2\} = \sum_{i=1}^n \{(\operatorname{Re} \lambda_i)^2 - (\operatorname{Im} \lambda_i)^2\} + \operatorname{tr}(HQ) \quad (2)$$

*Proof*

The Hamiltonian matrix is derived from optimal control theory by augmenting the co-states to the state space model. The Hamiltonian is

$$F = \begin{bmatrix} A & -H \\ -Q & -A^T \end{bmatrix} \in \mathbf{R}^{2n \times 2n} \quad (3)$$

$F$  has  $2n$  eigenvalues ( $n$  stable and  $n$  unstable) located symmetrically about the imaginary axis. The stable eigenvalues are identical to the eigenvalues of the closed-loop system matrix  $(A + BG) = (A - HR)$ , where  $G$  is the feedback matrix and  $R$  the symmetric solution of the algebraic Riccati equation. This can be seen from the following similarity transformation

$$\begin{bmatrix} I & 0 \\ R & I \end{bmatrix}^{-1} \begin{bmatrix} A & -H \\ -Q & -A^T \end{bmatrix} \begin{bmatrix} I & 0 \\ R & I \end{bmatrix} = \begin{bmatrix} A - HR & -H \\ 0 & -(A - HR)^T \end{bmatrix} \quad (4)$$

This means that the closed-loop eigenvalue spectrum can be derived from  $F$  without solving the algebraic Riccati equation.

Let  $\rho(F)$  denote the spectrum (set of  $2n$  eigenvalues) of  $F$ . Then we have that

$$\rho_i(F) = s_i, \quad i = 1, \dots, 2n \quad (5)$$

$$s_i = -s_{n+i}, \quad i = 1, \dots, n \quad (6)$$

$$\operatorname{tr}(F) = \sum_{i=1}^{2n} s_i = 0 \quad (7)$$

We also have that

$$\rho_i(F^2) = s_i^2, \quad i = 1, \dots, 2n \quad (8)$$

$$s_i^2 = s_{n+i}^2, \quad i = 1, \dots, n \quad (9)$$

$$\operatorname{tr}(F^2) = 2 \sum_{i=1}^n s_i^2 \quad (10)$$

We now need an expression for  $\operatorname{tr}(F^2)$ . We have

$$F^2 = \begin{bmatrix} A^2 + HQ & HA^T - AH \\ A^T Q - QA & (A^2 + HQ)^T \end{bmatrix} \quad (11)$$

From (11) we have

$$\operatorname{tr}(F^2) = \operatorname{tr}(A^2 + HQ) + \operatorname{tr}((A^2 + HQ)^T) = 2\operatorname{tr}(A^2 + HQ) \quad (12)$$

From (10) and (12) we get

$$\sum_{i=1}^n s_i^2 = \operatorname{tr}(A^2) + \operatorname{tr}(HQ) \quad (13)$$

and the theorem is proved.

$Q$  can be written as  $Q = S^T S$  ( $Q \geq 0$  and  $\text{rank}(S) = \text{rank}(Q)$ ). Then we have that

$$\text{tr}(HQ) = \text{tr}(HS^T S) = \text{tr}(SHS^T) \geq 0 \quad (14)$$

because the matrix  $SHS^T$  is symmetric and positive semidefinite. Combining (2) and (14) we deduce the inequality presented in Amin (1984) and partly in Koussiouris (1982), i.e.

$$\sum_{i=1}^n \{(\text{Re } s_i)^2 - (\text{Im } s_i)^2\} \geq \sum_{i=1}^n \{(\text{Re } \lambda_i)^2 - (\text{Im } \lambda_i)^2\} \quad (15)$$

An alternative way to establish the theorem is as follows. We have

$$(A - HR)^2 = (A - HR)(A - HR) = A^2 + H(-RA + RHR) - AHR \quad (16)$$

Combining equation (16) and the algebraic Riccati equation gives

$$(A - HR)^2 = A^2 + HQ + (HA^T - AH)R \quad (17)$$

Take the trace on both sides of equation (17), note that  $\text{tr}[(HA^T - AH)R] = 0$ , and equation (1) is proved.

The same procedure as above can be used to determine expressions for

$$\sum_{i=1}^n s_i^{2k}, \quad k = 1, 2, 3, \dots$$

For  $k=2$  we have

$$\begin{aligned} \sum_{i=1}^n s_i^4 &= \sum_{i=1}^n \{((\text{Re } s_i)^2 - (\text{Im } s_i)^2)^2 - 4(\text{Re } s_i)^2(\text{Im } s_i)^2\} \\ &= \text{tr}(A^4 + 4QA^2H - 2QAHA^T + (HQ)^2) \\ &= \text{tr}[(A^2 + HQ)(A^2 + HQ) + (A^TQ - QA)(HA^T - AH)] \end{aligned} \quad (18)$$

Finally, note that this procedure cannot be used to determine expressions for

$$\sum_{i=1}^n s_i^{2k-1}, \quad k = 1, 2, 3, \dots \quad (19)$$

because

$$\text{tr}(F^{2k-1}) = 0, \quad k = 1, 2, 3, \dots \quad (20)$$

### 3. Conclusions

A necessary condition is presented for the optimality of a linear multivariable feedback control system with respect to a quadratic performance index of infinite settling time.

#### REFERENCES

- AMIN, M. A. (1984). Further comments on 'A necessary condition for optimization in the frequency domain' and on 'Optimization and pole placement for a single input controllable system'. *International Journal of Control*, **40**, 863-865.
- DI RUSCIO, D., and BALCHEN, J. G. (1990). A Schur method for designing LQ-optimal systems with prescribed eigenvalues. *Modeling, Identification and Control*, **11**, 55-72.
- KOUSSIOURIS, T. G. (1982). A necessary condition for optimization in the frequency domain. *International Journal of Control*, **36**, 213-215.
- MAC FARLANE, A. G. J. (1970). Two necessary conditions in the frequency domain for the optimality of a multiple-input linear control system. *Proceedings IEEE*, **117**, 464-466.