Resource allocation by convex monotonous programming-application to an OTEC energy production platform

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A problem is considered of the minimization of a convex and monotonically increasing cost function subject to an upper bound of a convex and monotonically decreasing failure probability function. An algorithm is defined for the parametrical solution of the problem with respect to the selected failure probability level; the algorithm is applicable to problems with cost and failure probability functions that are not necessarily separable, thus extending a previously given algorithm for separable functions. A condition is given for the relaxation of the convexity assumption on the functions, and it is observed that the problem of the minimization of the failure probability subject to an upper bound on the total cost is solved simultaneously with the given problem. An analytically solvable numerical example is given and an application to the optimization of an OTEC energy production platform is briefly described, with reference to a complete description; it is concluded that the given extension of the algorithm to non-convex functions is important in this application.

1. Introduction

The work described in this paper was applied in the optimization of an OTEC-platform, used for offshore thermal energy conversion by harnessing the thermal gradients between the ocean surface and great depths. The work is described in detail in Fjeld, Stokke, Rønning, Mjelde, and Tvedt (1981). Several related aspects, including a model for inspection planning, are given by Sletten, Mjelde, Fjeld and Lotsberg (1982).

The motivation of the work is the high costs incurred in satisfying the requirements of a reliable structure. This makes it desirable to study the design of the structure in terms of a mathematical model of the minimization of the cost to obtain a selected reliability; this selected reliability level being varied parametrically in order to discuss the associated change of the total cost and the change of the design.

Methods of the allocation of resources to activities, see Mjelde (1983), are applied; in particular an algorithm of Luss and Gupta (1975) is extended to the problem discussed in this paper. Following a description of the model and the associated solution algorithm, the paper gives an analytically solvable example and a brief summary of an application to the optimization of an OTEC-platform.

2. Method of structural optimization

A concise mathematical discussion of the formulation and the solution of the optimization problem is given in this section.

Subject to a given geometry the structure is defined by a set of design variables, denoted by $W_1, ..., W_n$; and vectorized by $W = (W_1, ..., W_n)$. A cost function C(W)

is minimized subject to an upper bound on the structural failure probability $P_f(W)$. The resulting problem, denoted by Q, takes the form

Q: Minimize
$$z = C(W)$$

subject to the constraints

$$P_f(W) < P_f^*$$

and

where C(W) and $P_f(W)$ are convex and differentiable functions of W; C(W) is increasing and $P_f(W)$ is strictly decreasing in each component variable W_i for i=1, ..., n, and C(0)=0 and $P_f(0)\in\langle 0, 1\rangle$. The optimal objective value of Q is denoted by \bar{z} .

Defining the marginal cost to failure probability ratio $\eta_i(W)$ given by

$$\eta_i(W) = -\frac{\partial C}{\partial W_i} / \frac{\partial P_f}{\partial W_i}; \quad i = 1, ..., n$$

a feasible solution W of Q is optimal if and only if the following Kuhn-Tucker conditions are satisfactory for a subset A of $\{1, \ldots, n\}$ consisting of the indices i of design variables W_i with $W_i > 0$

$$\eta_i(W) = \lambda \quad \text{if } i \in A$$

$$\eta_i(W) > \lambda \quad \text{if } i \notin A$$

$$P_f(W) = P_f^* \tag{3}$$

where $\lambda > 0$ is a non-negative Langrange multiplier. The conditions state that the marginal return ratios $\eta_i(W)$ of all positive design variables are identical; a design variable W_i is zero if $\eta_i(W)$ is not sufficiently small. If P_f^* is replaced by P, the Lagrange multiplier λ of the Kuhn-Tucker conditions, when considered as a function of P, is denoted by $\lambda(P)$. A theorem of Everett (1963) demands that $\lambda(P)$ is monotonic in the following sense

$$P_1 < P_2 \Rightarrow \lambda(P_1) > \lambda(P_2) \tag{4}$$

The method of solution proposed in this paper is based on the application of the latter relationship to determine a value of λ that satisfies the Kuhn-Tucker conditions with $P = P_f^*$; this is achieved by increasing λ from the initial value

$$\lambda^0 = \min_{i=1, \dots, n} \eta_i(0)$$

to a value such that $P = P_f(W) = P_f^*$; a variable W_{i_1} such that $\eta_{i_1}(0) = \lambda^0$ starts to increase first; the variable W_{i_2} starts to increase at a value λ^1 of λ , where

$$\eta_{i_1}(W) = \eta_{i_2}(W) = \lambda^1$$

 $\eta_i(W) \ge \lambda^1 \quad \text{for } i \notin \{i_1, i_2\}$

where W satisfies $W_i = 0$ for $i \neq i_1$. As λ is increased, variables become positive when a relationship analogous to the one given above becomes satisfied. A variable at a positive value may also be reduced to zero again, when λ increases. The values of λ where a variable becomes positive or a positive variable is reduced to zero, are determined numerically by the application of Newton or gradient methods. The proposed

algorithm extends an algorithm of Luss and Gupta (1975) for the solution of a problem of the allocation of resources to activities in a case where C(W) and $P_f(W)$ are both separable functions; the present extension being applicable to functions C(W) and $P_f(W)$ that are not necessarily separable.

A value of λ where at least one W_i becomes positive or is reduced to zero is called respectively an in-point or an out-point. If the set $A = \{i \mid W_i > 0\}$ is denoted by $A(\lambda)$ for a given value of λ , it follows that λ is an in-out-point if and only if

$$A(\lambda - \epsilon) \neq A(\lambda + \epsilon)$$

for all sufficiently small values of $\epsilon > 0$, assuming that there is a finite number of in-out-points in a relevant interval of values of λ . An in-out-point satisfies the condition (1) with $W_i = 0$ for all $i \notin A$; an out-point satisfies the additional requirement that $W_i = 0$ for some $i \in A$; an in-point satisfies the requirement (2) as an equality for some $i \notin A$. For a given A this gives a set of equations for the possible in-out-points; the point with the smallest value of λ is selected. It follows that the in-out-points are generated in a sequence of increasing values of λ . When an in-out-point λ with an associated W such that $P_f(W) \leq P_f^*$ has been obtained, a solution of the problem Q for a given value of P_f^* is determined by the simultaneous solution of eqns. (1) and (3) with $W_i = 0$ for $i \notin A$. All the previously mentioned sets of equations are solved by any convenient method, such as a Newton or a gradient method; a numerical example with analytically solvable equations is given in the following section of this paper.

It is noted that the fundamental assumption of the previously given algorithm is the condition (4); the algorithm is applicable if this condition is satisfied and if there corresponds a uniquely determined value of W to each value of λ . The implication is that the applicability of the algorithm includes cases where C(W) or $P_f(W)$ is not necessarily convex, such as the OTEC optimization given in the final section of this paper.

The algorithm solves two related problems simultaneously; the given problem Q and the problem of the minimization of $P_f(W)$ subject to an upper bound of C(W); if $\bar{z} = C(W)$ is the minimal cost for a given $P_f(W) = P_f^*$ it follows, from the Kuhn-Tucker optimality conditions of the two related problems, that $P_f^* = P_f(W)$ is minimal for $C(W) \leq \bar{z}$.

It is important that the algorithm gives a sensitivity analysis of the solution of Q for selected values of P; the optimal value of Q as a function of P is denoted by h(P), thus

$$\bar{z} = C(W) = h(P)$$

The latter relationship, when combined with the economical consequences of a failure, can be used to determine an economically optimal failure probability P by the minimization of the total costs given by

$$C_T = h(P) + P \cdot C_f$$

where C_f is the cost of failure. It is understood that the design variables W_i for i=1, ..., n of the problem Q determine initial costs, and expected costs of inspection and maintenance as parts of h(P). Furthermore, the cost h(P) and the probability P refer to a given length of time, for instance a year and a given interest rate and a given taxation system.

The value of P_f^* in the problem Q must be chosen such that:

$$P_f^* < \overline{P}$$

when factors such as a possible loss of human lives or public recognition are considered. The effect of the approach is to avoid cheap elements with a high failure probability, and to avoid costly elements with a low failure probability, since such elements

contradict the optimality conditions and represent respectively weak links and over-

designed elements.

3. Numerical example

A simple numerical example with n=2 is given as follows

$$C(W) = \sum_{i=1}^{n} W_{i}$$

$$P_{f}(W) = P_{f0} \left[1 - \sum_{k=1}^{K} r_{k} \left(\sum_{i=1}^{n} \gamma_{ik} W_{i} \right) \right]$$

where P_{f0} is an unknown constant, K=2 and the other data are given by

$$r_k(\epsilon_k) = s_k \epsilon_k - m_k \epsilon_k^2; \quad \epsilon_k < s_k / 2m_k; \quad k = 1, 2$$

$$(s_1, s_2) = (1 \cdot 3, 1 \cdot 0)$$

$$(m_1, m_2) = (3 \cdot 0, 1 \cdot 0)$$

$$(\gamma_{ik}) = \begin{pmatrix} 1 \cdot 0 & 0 \cdot 5 \\ 0 \cdot 5 & 1 \cdot 0 \end{pmatrix}$$

it follows that the expressions for $r_k(\epsilon_k)$ for k=1, 2 are valid for $\epsilon_1 < 0.217$ and $\epsilon_2 < 0.50$. The solution of the problem Q is given in Table 1 for three values of the cost C.

C	W_1	W_2	P_f/P_{f0}	
0.06	0.06	0	0·9037 0·6625 0·6200	
0.30	0	0.30		
0.40	0	0.40		

Table 1. Numerical example.

When C increases from C=0 to C=0.06, the value of W_1 increases from 0 to 0.06 with $W_2 = 0$; a further increase of C causes W_1 to decrease and W_2 to increase until W_1 becomes zero when $W_2 = 0.30$; if C is increases in the interval [0.30, 0.40] the value of W_1 stays at zero and W_2 increases to $W_2 = 0.40$. The table contains an in-point for C=0.06 and an out-point for C=0.30.

4. Application to an OTEC platform

Fjeld, Stokke, Rønning, Mjelde, and Tvedt, (1981) applied the previously given algorithm to the cost-benefit analysis of the design of an OTEC platform, in terms of the following design variables

 W_1 : static strength

W2: redundance

 W_3 : fatigue strength

 W_4 : in-service inspection, damage

W₅: in-service inspection, warning

W₆: fabrication control, gross errors

 W_7 : fabrication control, fatigue

where the following normalizations are applied; $W_i \in [0, 1]$ for i = 1, 3, 5, 6, 7; $W_2 \in [1, 3]$ and $W_4 \in [0.01, 1]$.

The cost is expressed as

$$C = C_0(C_1 + C_2 + C_3 + C_4 + C_5(1 + P_{f \text{ local }} C_8) + C_6 + C_7)$$

where C_0 is the cost of some base case and C_t are coefficients describing the cost variations by increasing efforts to improve the safety, and the probability $P_{f \text{ local}}$ is defined below.

The expressions for the C_i are

$$C_i = A_i W_i$$
 for $i = 1, 3, 4, 5, 6, 7$

$$C_2 = 1 + w_2^{2\cdot 5}/A_2$$

$$C_{\rm R} = A_{\rm R}$$

for constants A_1 , i=1, ..., 8.

The probability of failure is expressed as

$$P_f = P_{f \text{ local}} \cdot \phi_2 \cdot \phi_4$$

where the probability of local failure $P_{f \text{ local}}$ is given by

$$P_{f \text{ local}} = P_{of \text{ gross error}} \cdot \phi_6 + P_{of \text{ accident}} + P_{of \text{ static}} \cdot \phi_1 + P_{of \text{ fatigue}} \cdot \phi_3 \cdot \phi_5 \cdot \phi_7$$

The P_{of} are failure probabilities for four independent failure reasons in an 'initial' situation i.e. before any of the safety measures/design variables are applied.

Expressions for the ϕ_i are given in Table 2, where the B_i for i=1, ..., 7 are constants.

The constants A_i , B_i and the P_{of} in a numerical case are given in Table 3.

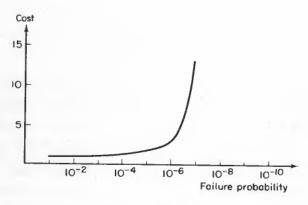
The Figure gives a sensitivity analysis of cost versus failure probability.

Since the failure probabilities are estimated only in a relative sense, a sensitivity analysis, such as that given in the Figure, provides important information for a decision on the total cost level of the structure: in the example of the Figure a cost above the level from 2 to 3 will only marginally decrease the failure probability.

In this particular example the applicability of the algorithm was checked by the validity of condition (4) and the unique solvability of all the equations involved for a set of initial conditions, or there was no solution; the check was performed for an increasing sequence of values of λ . This check was applied, rather than deciding on the

	Design variable			ϕ_i				
	Static	strength		$\phi_1 = 1$	$0^{-B_1w_1}$	19.56		
	Redundance Fatigue strength			$\phi_2 = B$				
				$\phi_3 = (1$	$(1+w_3)^{-B}$	3		
		In-service inspection, damage			$-B_4\sqrt{w_4}$			
	In-service inspection, warning Fabrication control, gross error			$\phi_5 = 1$	$-B_5 \frac{1-a}{1-a}$	$\frac{e^{-w_5}}{e^{-1}}$		
				$\phi_6 = \frac{1}{\sqrt{1}}$	$\frac{B_6}{/[B_6^2+w]}$	<u></u>]		
		Fabrication control, fatigue			$\phi_7 = \frac{B_7}{(B_7 + w_7)^2}$			
			Table 2.	The fund	ctions ϕ_i .			
i	1	2	3	4	5	6	7	
A_{l}	0.8	16	0-2	10	10	0.03	0.1	10
B_i	3	10	12	0.9	0.9	0.1	0.01	
	oss error	P_o	f accident		P _{of static}	:	P _{of fat}	igue

Table 3. Values of A_i , B_i and P_{of} .



Sensitivity analysis

question of the convexity of $P_f(W)$ in a given region for the functions $\phi_i(W)$ defined in Table 2 (since the product of two convex functions is not necessarily convex, as exemplified by the product $(4-W_1)$ $(4-W_2)$ and the points $(W_1, W_2)=(2, 2)$, (1, 3) $(1\cdot 5, 2\cdot 5)$). However, for exponential functions $\phi_i(W_i)=a_i\exp(-\alpha_iW_i)$ the convexity of $P_f(W)$ is obvious, such functions appear if the relationship $\phi_i^1(W_i)=-\alpha_i\phi_i(W_i)$ is

applicable, where ϕ^1_i is the derivative of ϕ_t . Also note that, even for exponential functions $\phi_i(W_i)$, the convexity of C(W) is not clear due to the term $C_5 \cdot (1 + P_{f \text{ local }} C_8)$. It is therefore a particular advantage of the method proposed in this paper that cases with non-convex functions can be treated without much difficulty, subject to a confirmative check of the validity of condition (4).

The numerical example given here is only one of a large set of numerical cases discussed in Fjeld, Stokke, Rønning, Mjelde and Tvedt (1981): these cases constitute a sensitivity analysis of the problem with respect to variations of the parameters within their respective uncertainty-ranges.

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